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(54) POSTERIOR STABILIZED ORTHOPAEDIC PROSTHESIS

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(56) References Cited

U.S. PATENT DOCUMENTS

3,765,033 A	10/1973	Goldberg et al.				
3,840,905 A	10/1974	Deane				
3,852,045 A	12/1974	Wheeler				
3,855,638 A	12/1974	Pilliar				
3,869,731 A	3/1975	Waugh et al.				
4,081,866 A	4/1978	Upshaw et al.				
4,156,943 A	6/1979	Collier				
	(Continued)					

FOREIGN PATENT DOCUMENTS

CN 1803106 A 7/2006 CN 1872009 A 12/2006 (Continued) OTHER PUBLICATIONS

State Intellectual Property Office of People's Republic of China; Chinese Search Report; Application No. 200910166935.6; Mar. 26, 2013, 2 pages.

(Continued)

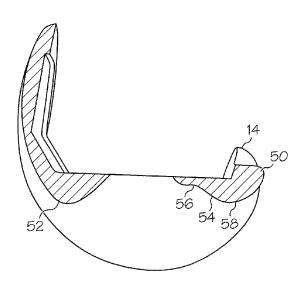
Primary Examiner — David H Willse Assistant Examiner — Javier Blanco

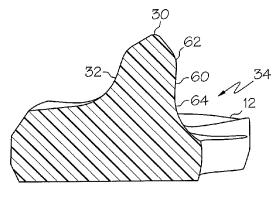
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(57) ABSTRACT

A posterior stabilized knee orthopaedic prosthesis includes a tibial bearing and a femoral component configured to articulate with the tibial bearing. The tibial bearing includes a spine having a concave cam surface and a convex cam surface. The femoral component includes a posterior cam having a concave cam surface and a convex cam surface. During flexion, the concave cam surface of the posterior cam contacts the convex cam surface of the spine and the convex cam surface of the spine.

12 Claims, 12 Drawing Sheets





US 9,204,968 B2 Page 2

(56)		Referen	ces Cited	5,702,464			Lackey et al.
	ЦS	PATENT	DOCUMENTS	5,702,466 5,725,584			Pappas et al. Walker et al.
	0.6.	171111111	DOCOMENTS	5,728,748	A	3/1998	Sun
	206,516 A	6/1980		5,732,469			Hamamoto
	209,861 A		Walker et al.	5,755,800 5,755,801		5/1998 5/1998	Walker et al.
	215,439 A 249,270 A		Gold et al. Bahler et al.	5,755,803			Haines et al.
	257,129 A	3/1981		5,765,095		6/1998	
	262,368 A	4/1981		5,766,257 5,776,201			Goodman et al. Colleran et al.
	340,978 A 470,158 A		Buechel et al. Pappas et al.	5,800,552		9/1998	
	612,160 A		Donlevy	5,811,543			Hao et al.
	673,407 A	6/1987		5,824,096 5,824,100			Pappas et al. Kester et al.
	714,474 A 795,468 A		Brooks, Jr. Hodorek	5,824,100			Buscayret
	808,185 A		Penenberg et al.	5,824,103		10/1998	Williams
	822,362 A	4/1989		5,871,543 5,871,545			Hofmann Goodfellow
	838,891 A 888,021 A		Branemark Forte et al.	5,871,546		2/1999	Colleran et al.
	938,769 A	7/1990		5,879,394	A	3/1999	Ashby
4,	944,757 A	7/1990	Martinez	5,879,400		3/1999	
	944,760 A	7/1990		5,906,644 5,935,173		5/1999 8/1999	Roger et al.
	950,298 A 963,152 A		Gustilo et al. Hofmann et al.	5,951,603	A	9/1999	O'Neil et al.
4,	990,163 A	2/1991	Ducheyne	5,957,979			Beckman
	007,933 A		Sidebotham et al.	5,964,808 5,976,147		10/1999	LaSalle et al.
	011,496 A 019,103 A		Forte et al. Van Zile	5,984,969		11/1999	Matthews
5,	037,423 A	8/1991	Kenna	5,989,027		11/1999	
	071,438 A		Jones et al.	5,997,577 6,004,351		12/1999	Herrington et al. Tomita et al.
	080,675 A 104,410 A	1/1992 4/1992	Lawes Chowdhary	6,005,018			Cicierega
	108,442 A	4/1992		6,010,534	A	1/2000	O'Neil et al.
	116,375 A		Hofmann	6,013,103 6,017,975		1/2000 1/2000	Kaufman et al.
	133,758 A 147,405 A		Hollister Van Zile et al.	6,039,764			Pottenger et al.
	171,283 A	12/1992		6,042,780	A	3/2000	Huang
5,	201,766 A	4/1993	Georgette	6,053,945 6,059,949		4/2000 5/2000	O'Neil et al.
	219,362 A 236,461 A	6/1993 8/1993	Tuke et al.	6,068,658		5/2000	
	251,468 A	10/1993		6,080,195	A	6/2000	Colleran et al.
5,	258,044 A	11/1993		6,090,144		7/2000	
	271,737 A 282,861 A	12/1993 2/1994	Baldwin	6,123,728 6,123,729			Brosnahan et al. Insall et al.
	308,556 A	5/1994		6,123,896	A	9/2000	Meeks, III
5,	309,639 A	5/1994	Lee	6,126,692			Robie et al.
	326,361 A	7/1994 7/1994	Hollister Wellson	6,135,857 6,139,581		10/2000	Shaw Engh et al.
	330,533 A 330,534 A		Herrington et al.	6,152,960		11/2000	
5,	344,460 A	9/1994	Turanyi et al.	6,162,254	A	12/2000	Timoteo
	344,461 A	9/1994	Phlipot Davidson	6,174,934 6,206,926		1/2001 3/2001	Sun Pappas
	344,494 A 358,527 A	10/1994		6,210,444		4/2001	Webster
5,	368,881 A	11/1994	Kelman	6,210,445			Zawadzki
	370,699 A		Hood et al.	6,217,618 6,228,900		5/2001	Hileman Shen
	387,240 A 395,401 A	2/1995 3/1995	Pottenger et al. Bahler	6,238,434		5/2001	
5,	405,396 A	4/1995	Heldreth et al.	6,242,507		6/2001	
	413,604 A	5/1995		6,245,276 6,258,127			McNulty Schmotzer
	414,049 A 449,745 A	5/1995 9/1995		6,264,697		7/2001	
	458,637 A	10/1995	Hayes	6,280,476			Metzger
	480,446 A		Goodfellow	6,281,264 6,299,646		8/2001 10/2001	Salovey Chambat et al.
	543,471 A 549,686 A	8/1996 8/1996	Johnson et al.	6,316,158		11/2001	
5,	571,187 A		Devanathan	6,319,283		11/2001	
	571,194 A	11/1996		6,325,828 6,344,059			Dennis et al. Krakovits et al.
	609,639 A 609,643 A	3/1997 3/1997	Walker Colleran et al.	6,361,564			Marceaux
5,	639,279 A	6/1997	Burkinshaw et al.	6,372,814	В1	4/2002	Sun
	650,485 A	7/1997		6,379,388			Ensign et al.
	658,333 A 658,342 A		Kelman Draganich et al.	6,428,577 6,443,991			Evans et al. Running
	658,344 A		Hurlburt	6,475,241		11/2002	
5,	681,354 A	10/1997	Eckhoff	6,485,519	B2	11/2002	Meyers et al.
	683,468 A	11/1997		6,491,726		12/2002	
	702,458 A 702,463 A	12/1997 12/1997	Burstein et al.	6,494,914 6,503,280			Brown et al. Repicci
3,	702,703 A	14/177/	1 Ounci	0,505,200	202	1/2003	Repieer

US 9,204,968 B2 Page 3

(56)		Referen	ces Cited	7,749,229	B1		Bonutti
	US	PATENT	DOCUMENTS	7,753,960 7,771,484			Cipolletti et al. Campbell
	0.0		DOCUMENTS	7,776,044			Pendleton
	215 B1	1/2003	Letot	7,806,896		10/2010	
	216 B1		McCue	7,806,897 7,837,736		10/2010 11/2010	
	522 B2 787 B2	2/2003	Vaidyanathan Biegun et al.	7,842,093			Peters et al.
	426 B1	5/2003		7,875,081			Lipman et al.
	202 B2		Whiteside	7,922,771			Otto et al.
	469 B1		Tornier	8,187,335 8,192,498			Wyss et al. Wagner et al.
	470 B1 283 B1	6/2003	Lee Metzger et al.	8,784,496			Wagner et al.
	787 B2	7/2003	Pickrell	8,795,380	B2	8/2014	Heldreth et al.
6,620,	198 B2		Burstein et al.	8,828,086			Williams et al.
	526 B1	9/2003		8,834,575 2002/0138150			Wyss et al. Leclercq
	251 B2 039 B1		Salehi et al. Evans et al.	2003/0009232			Metzger et al.
	224 B2		Lefebvre	2003/0035747			Anderson
	308 B2	12/2003		2003/0044301 2003/0075013			Lefebvre Grohowski
	821 B2		Bonutti	2003/00/3013		7/2003	
	800 B2 724 B2		Meyers et al. Repicci	2003/0153981		8/2003	Wang
	128 B2	5/2004	Burstein	2003/0171820			Wilshaw
	516 B2	7/2004		2003/0199985 2003/0212161		10/2003	Masını McKellop
	078 B2 099 B2		Bonutti Andriacchi et al.	2003/0212101		12/2003	
	461 B2		Meyers et al.	2004/0015770			Kimoto
	005 B2	9/2004		2004/0039450			Griner et al.
	020 B2	11/2004		2004/0167633 2004/0186583		8/2004 9/2004	
	327 B2 329 B2		Khandkar McMinn	2004/0215345		10/2004	
	230 B1		Feichtinger	2004/0243244			Otto et al.
6,852,	272 B2	2/2005	Artz	2004/0243245			Plumet et al. Tarabichi
	148 B2		Tuke et al.	2005/0021147 2005/0055102		3/2005	
	388 B2 467 B1		Reising et al. Bercovy	2005/0059750		3/2005	
	340 B2		Metzger et al.	2005/0069629		3/2005	
	832 B1		Sharkey	2005/0096747 2005/0100578			Tuttle et al. Schmid
	738 B2 570 B2	8/2005 9/2005	Wyss Heldreth et al.	2005/0100578		6/2005	
	039 B2		Metzger et al.	2005/0143832		6/2005	
6,986,	791 B1	1/2006	Metzger	2005/0154472		7/2005	
	788 B2		Metzger et al.	2005/0203631 2005/0209701		9/2003	Daniels Suguro et al.
	741 B2 963 B2		Swanson Naegerl	2005/0209702		9/2005	
7,070,0	522 B1	7/2006		2005/0249625		11/2005	
	137 B1		Servidio	2005/0278035 2006/0002810			Wyss et al. Grohowski
	259 B2 401 B2	8/2006 9/2006	Tarabichi Brack	2006/0002810			Chambat et al.
	996 B2		Bonutti	2006/0036329	A1		Webster
7,105,0	D27 B2	9/2006	Lipman et al.	2006/0052875			Bernero
	319 B2	12/2006		2006/0100714 2006/0178749		5/2006 8/2006	Pendleton et al.
7,100,. 7,175,0	330 B2 565 B2		Axelson, Jr. et al. German	2006/0195195		8/2006	Burstein
	715 B2		Metzger	2006/0228247			Grohowski
	740 B2		Tuttle et al.	2006/0231402 2006/0241781		10/2006 10/2006	
	164 B2 252 B2		Johnson et al. Otto et al.	2006/0257358		11/2006	
	502 B2		Fell et al.	2006/0271191	A1	11/2006	Hermansson
7,344,	460 B2	3/2008	Gait	2006/0289388		12/2006	
	817 B2		D'Alessio, II	2007/0061014 2007/0073409			Naegerl Cooney
	505 B2 557 B1		Burseein et al. Bonutti	2007/0078521			Overholser
	550 B2		Johnson et al.	2007/0100463		5/2007	
	292 B2		Crabtree et al.	2007/0129809 2007/0135926		6/2007 6/2007	Meridew Walker
	850 B2 079 B1		Kuczynski et al. Blackwell et al.	2007/0133920			Meridew
	519 B2		Lefevre et al.	2007/0196230			Hamman
7,615,0	054 B1	11/2009	Bonutti	2007/0203582			Campbell
	462 B2	11/2009		2007/0219639			Otto et al.
	818 B2 390 B1	12/2009	Hazebrouck et al.	2007/0293647 2008/0004708		1/2007	McKellop Wyss
	767 B2	2/2010		2008/0004708			Peters et al.
	151 B2	3/2010		2008/0091272	A1	4/2008	
	152 B2		Suguro et al.	2008/0097616		4/2008	Meyers et al.
	740 B1		Bonutti	2008/0114462		5/2008	Guidera et al.
	741 B1 562 B2		Bonutti Barnett et al.	2008/0114464 2008/0119940			Barnett et al. Otto et al.
7,740,0	JUL D L	0/2010	Darnett et al.	2000/0119940	2 3 1	5/2000	ono et al.

(56)	Referen	ices Cited		EP	883388	12/1998	
11.6	DATENIT	DOCUMENTS		EP EP	634156 1374805	5/1999 1/2001	
0.,	S. PALENT	DOCUMENTS		EP	1129676	9/2001	
2008/0161927 A1	7/2008	Savage		EP	636352 B1	1/2002	
2008/0195108 A1	8/2008	Bhatnagar et al.		EP	1196118	4/2002	
2008/0199720 A1				EP EP	765645 1421918 A1	8/2003 5/2004	
2008/0206297 A1 2008/0269596 A1		Roeder Revie et al.		EP	1440675	7/2004	
2009/0043396 A1		Komistek		EP	1470801	10/2004	
2009/0048680 A1		Naegerl		EP EP	732092	2/2005	
2009/0082873 A1		Hazebrouck		EP EP	1518521 A2 1226799	3/2005 5/2005	
2009/0084491 A1 2009/0088859 A1		Uthgenannt Hazebrouck et al.		EP	1591082	11/2005	
2009/0125114 A1		May et al.		EP	1779812 A1	5/2007	
2009/0192610 A1				EP EP	1923079 A1 2649965 A1 ³	5/2008	
2009/0265012 A1		Engh et al. Mandell		FR	2417971	2/1979	
2009/0265013 A1 2009/0292365 A1				FR	2621243	4/1989	
2009/0295035 A1				FR	2653992 A1	5/1991	
2009/0306785 A1		Farrar et al.		FR FR	2780636 A1 2787012	1/2000 6/2000	
2009/0319047 A1		Walker		FR	2809302 A1	11/2001	
2009/0326663 A1 2009/0326664 A1		Wagner et al.		FR	2835178	8/2003	
2009/0326665 A1		Wyss et al.		GB	1065354 A	4/1967	
2009/0326666 A1		Wyss et al.		GB GB	2293109 A 2335145 A	3/1996 9/1999	
2009/0326667 A1 2009/0326674 A1		Williams et al.		JP	62205201 1 A	9/1999	
2010/0016979 A1		Wyss et al.		JP	2004167255	2/1996	
2010/0036499 A1		Pinskerova		JP	08224263 A	9/1996	
2010/0036500 A1		Heldreth		JP JP	2002291779 A 2004167255	10/2002	
2010/0042224 A1		Otto et al.		JP JP	2004107233 2006015133 A	6/2004 1/2006	
2010/0042225 A1 2010/0063594 A1		Hazebrouck		WO	7900739	10/1979	
2010/0070045 A1				WO	8906947	8/1989	
2010/0076563 A1		Otto et al.		WO WO	9014806 A1	12/1990	
2010/0076564 A1		Schilling et al.		WO	9601725 9623458	1/1996 8/1996	
2010/0094429 A1 2010/0098574 A1				WO	9624311	8/1996	
2010/0100189 A1	4/2010	Metzger		WO	9624312	8/1996	
2010/0100190 A1	4/2010	May		WO WO	9846171	10/1998	
2010/0100191 A1		May et al.		WO	9927872 9966864 A1	6/1999 12/1999	
2010/0125337 A1 2010/0161067 A1		Grecco et al. Saleh et al.		WO	0209624	2/2002	
2010/0191341 A1				WO	03039609 A1	5/2003	
2010/0222890 A1		Barnett		WO WO	03101647 A2 2004058108	12/2003 7/2004	
2010/0286788 A1 2010/0292804 A1		Komistek		WO	2004058108	8/2004	
2010/0292804 A1 2010/0305710 A1		Samuelson Metzger		WO	2005009489 A2	2/2005	
2010/0312350 A1		Bonutti		WO	2005009729 A2	2/2005	
2011/0029090 A1		Zannis		WO WO	2005072657 2005087125	8/2005 9/2005	
2011/0029092 A1 2011/0035017 A1		Deruntz Deffenbaugh		WO	2005087125 2006014294 A1	2/2006	
2011/0035017 A1 2011/0035018 A1		Deffenbaugh		WO	2006130350 A2	12/2006	
2011/0106268 A1		Deffenbaugh		WO	2007106172	9/2007	
2011/0118847 A1		Lipman et al.		WO WO	2007106172 A 2007108804	9/2007 9/2007	
2011/0125280 A1		Otto et al.		WO	2007119173	10/2007	
2011/0153026 A1		Heggendorn et al.		WO	2008100784 A2	8/2008	
2012/0239158 A1 2012/0259417 A1		Wagner et al. Wyss et al.		WO WO	2009046212 A2	4/2009	
2012/0271428 A1		Heldreth et al.		WO	2009128943 A2	10/2009	
2012/0296437 A1	11/2012	Wyss et al.			OTHER PUI	BLICATIONS	}
2013/0006372 A1		Wyss et al.		_			
2013/0006373 A1		Wyss et al.			Search Report for E	-	it Application No.
2014/0243987 A1 2014/0303740 A1		Wagner et al. Heldreth et al.			5-1526, Dec. 22, 2009		
2014/0350686 A1		Williams et al.			Search Report for E		it Application No.
2015/0005888 A1		Wyss et al.			8-1526, Jan. 4, 2010, 6 Search Report for F		t Application No
					5-1526, Jan. 4, 2010, 4		и Аррисанов №.
FORE	IGN PATE	NT DOCUMENTS			Search Report for H		t Application No.
DE 42005/2 0/1004			-	0-1526, Feb. 2, 2010,	-	11	
	308563 529824	9/1994 2/1997		Biomet, Va	nguard Mono-Lock T	ibial System, P.	atented Convertible
	510178	5/1992		Tibial Bear	ring Technology, 2009	, 2 Pages.	G 6 M :
	495340 A1	7/1992			Zeiss Surfcomm 5000	—"Contour and	Surface Measuring
	634155 636352 A2	1/1995 2/1995			, 2005, 16 pages. ., "AMK Total Knee S	vstem Product	Brochure" 1996 &
	732091	2/1995 9/1996		pages.	., ANTE TOTAL INICE S	y stern i roduct	1330, 6
		2,1220		L2-2.			

(56) References Cited

OTHER PUBLICATIONS

DePuy Knees International, "Sigma CR Porocoat®," 1 page.

DePuy Orthopaedics, Inc., "AMK Total Knee System Legent II Surgical Techinque", 1998, 30 pages.

DePuy Orthopaedics, Inc., "Sigma Fixed Bearing Knees—Function with Wear Resistance", 2010, 0612-65-508 (Rev. 1) 20 pages.

DePuy PFC Sigma RP, "PFC Sigma Knee System with Rotating Platform Technical Monograph", 1999, 0611-29-050 (Rev. 3), 70 pages.

Effects of Coronal Plane Conformity on Tibial Loading in TKA: A Comparison of AGC Flat Versus Conforming Articulations, Brent, et al, Orthopaedic Surgery, Surgical Technology International, XVIII, 6 pages.

European Search Report for European Patent Application No. 09164245.4-2310, Oct. 15, 2009, 5 pgs.

European Search Report for European Patent Application No. 08253140.1-2310, Dec. 23, 2008, 7 pgs.

European Search Report for European Patent Application No. 11150648.1-2310, Apr. 7, 2011, 4 pages.

European Search Report for European Patent Application No. 06739287.8-2310, Mar. 16, 2010, 3 Pages.

European Search Report for European Patent Application No. 09164478.1-2310, Oct. 20, 2009, 6 Pages.

European Search Report for European Patent Application No. 09164478.1-2310, Apr. 28, 2010, 12 Pages.

European Search Report for European Patent Application No. 10162138.1, Aug. 30, 2010, 7 Pages.

Japanese Search Report for Japanese Patent Application No. 2009-501393, Oct. 26, 2010, 5 Pages.

PCT Notification Concerning Transmittal of International Prel. Report for Corresponding International App. No. PCT/US2006/010431, Jun. 5, 2007, 89 Pages.

Procedure, References Guide for Use with P.F.C. Sigma Knee Systems, 1998, 8 pages.

Signus Medizintechnik, "PEEK-OPTIMA®, The Polymer for Implants, Technical Information for the Medical Professional", 7

The Effects of Conformity and Load in Total Knee Replacement, Kuster, et al, Clinical Orthopaedics and Related Research No. 375, Jun. 2000

Zimmer Nexgen Trabecular Metal Tibial Tray, The Best Thing Next to Bone, 97-5954-001-00, 2007, 4 pages.

Zimmer, Trabecular Metal Monoblock Tibial Components, An Optimal Combination of Material and Design, www.zimmer.com, 2009, 3 pages.

European search report; European Application No. 10174439.9-1526; Dec. 20, 2010; 4 pages.

"Vanguard Complete Knee System," Biomet, available at: http://www.biomet.com/patients/vanguard_complete.cfm, downloaded on Feb. 2009, (3 pages).

"NexGen Complete Knee Solution Cruciate Retaining Knee (CR)," Zimmer, available at: http://zimmercom.au/ctl?template=PC&op=global&action=&template=PC&id=356, downloaded on Feb. 18, 2009, (1 page).

Scorpio Knee TS Single Axis Revision Knee System, Stryker Orthopaedics, http://www.stryker.com/stellent/groups/public/documents/web_prod/023609.pdf, (6 pages).

P. Johal et al, "Tibio-femoral movement in the living knee. A study of weight bearing and non-weight bearing knee kinematics using 'interventional' MRI," Journal of Biomechanics, vol. 38, Issue 2, Feb. 2005, pp. 269-276, (8 pages).

Andriacchi, T.P., "The Effect of Knee Kinematics, Gait and Wear on the Short and Long-Term Outcomes of Primary Knee Replacement," NIH Consensus Development Conference on Total Knee Replacement, pp. 61-62, Dec. 8-10, 2003, (4 pages).

Asano et al. "In Vivo Three-Dimensional Knee Kinematics Using a Biplanar Image-Matching Technique," Clin Orthop Rel Res, 388: 157-166, 2001, (10 pages).

Kessler et al., "Sagittal curvature of total knee replacements predicts in vivo kinematics," Clinical Biomechanics 22(1): 52-58, 2007.

Wang et al., "Biomechanical differences exhibited during sit-to-stand between total knee arthroplasty designs of varying radii," J Arthroplasty 21(8): 1196-9, 2006.

Saari et al., "The effect of tibial insert design on rising from a chair; motion analysis after total knee replacement," Clin Biomech 19(9): 951-6, 2004.

Ranawat, "Design may be counterproductive for optimizing flexion after TKR," Olin Orthop Rel Res 416: 174-6, 2003.

D'Lima et al., "Quadriceps moment arm and quadriceps forces after total knee arthroplasty," Clin Orthop Rel Res 393:213-20, 2001.

Uvehammer et al., "In vivo kinematics of total knee arthroplasty: flat compared with concave tibial joint surface," J Orthop Res 18(6): 856-64, 2000.

Dennis et al., "In vivo anteroposterior femorotibial translation of total knee arthroplasty: a multicenter analysis," Olin Orthop Rel Res, 356: 47-57, 1998.

Clary et al., "Kinematics of Posterior Stabilized and Cruciate Retaining Knee Implants During an in Vitro Deep Knee Bend," 54th Annual Meeting of the Orthopaedic Research Society, Poster No. 1983, Mar. 2008.

Wang et al., "A biomechanical comparison between the single-axis and multi-axis total knee arthroplasty systems for stand-to-sit movement," Clin Biomech 20(4): 428-33, 2005.

Dennis et al., "Multicenter Determination of in Vivo Kinematics After Total Knee Arthroplasty," Clin. Orthop. Rel. Res., 416, 37-57, 21 pgs.

Yoshiya et al., "In Vivo Kinematic Comparison of Posterior Cruciate-Retaining and Posterior Stabilized Total Knee Arthroplasties Under Passive and Weight-bearing Conditions," J. Arthroplasty, vol. 20, No. 6, 2005, 7 pgs.

Bertin et al., "In Vivo Determination of Posterior Femoral Rollback for Subjects Having a NexGen Posterior Cruciate-Retaining Total Knee Arthroplasty," J. Arthroplasty, vol. 17, No. 8, 2002, 9 pgs.

Suggs et al., "Three-Dimensional Tibiofemoral Articular Contact Kinematics of a Cruciate-Retaining Total Knee Arthroplasty," JBJS-Am, vol. 88, No. 2, 2006, 10 pgs.

Dennis et al., "In Vivo Determination of Normal and Anterior Cruciate Ligament-Deficient Knee Kinematics," J. Biomechanics, 38, 241-253, 2005, 13 pgs.

Li et al., "Anterior Cruciate Ligament Deficiency Alters the In Vivo Motion of the Tibiofemoral Cartilage Contact Points in Both Anteroposterior and Mediolateral Directions," JBJS-Am, vol. 88, No. 8, Aug. 2006, 10 pgs.

Ries, "Effect of ACL Sacrifice, Retention, or Substitution on K After TKA," http://www.orthosupersite.com/view.asp?rID=23134, Aug. 2007, 5 pgs.

Ferris, "Matching observed spiral form curves to equations of spirals in 2-D images, "The First Japanese-Australian Joint Seminar, 7 pgs. Goodfellow et al., "The Mechanics of the Knee and Prosthesis Design," The Journal of Bone and Joint Surgery, vol. 60-B, No. 3, 12 pgs.

Zimmer Nexgen Trabecular Metal Tibial Tray, "The Best Thing Next to Bone", 97-5954-001-00, 2007, 4 pages.

European Search Report for European Patent Application No. 08164944.4-2310-2042131, Mar. 16, 2009, 12 pgs.

Shaw et al., "The Longitudinal Axis of the Knee and the Role of the Cruciate Ligaments in Controlling Transverse Rotation", J. Bone Joint Surg. Am 1974:56:1603-1609, 8 pages (1974).

Kurosawa, et al., "Geometry and Motion of the Knee for Implant and Orthotic Design", The Journal of Biomechanics 18 (1985), pp. 487-499, 12 pages.

Barnes, C.L., et al, "Kneeling Is Safe for Patients Implanted With Medical-Pivot Total Knee Arthoplasty Designs, Journal of Arthoplasty", vol. 00, No. 0 2010, 1-6, 6 pages (2010). Blaha, et al., "Kinematics of the Human Knee Using an Open Chain

Blaha, et al., "Kinematics of the Human Knee Using an Open Chain Cadaver Model", Clinical Orthopaedics and Related Research, vol. 410 (2003); 25-34, 10 pages.

Dennis, et al. "A Multi-Center Analysis of Axial Femorotibial Rotation After Total Knee Arthoplasty", Clinical Orthopaedics 428 (2004); 180-189, 10 pages.

Fan, Cheng-Yu, et al., "Primitive Results After Medical-Pivot Knee Arthroplasties: A Minimum 5 Year Follow-Up Study", The Journal of Arthroplasty, vol. 25, No. 3 2010, 492-496, 5 pages (2010).

(56) References Cited

OTHER PUBLICATIONS

Freeman, M.A.R., et al., "The Movement of the Normal Tibio-Femoral Joint", The Journal of Biomechanics 38 (2005) (2), pp. 197-208, 12 pgs.

Fuller, et al., "A Comparison of Lower-Extremity Skeletal Kinematics Measured Using Skin and Pin-Mounted Markers", Human Movement Science 16 (1997) 219-242, 24 pages.

Hill, et al., "Tibiofemoral Movement 2: The Loaded and Unloaded Living Knee Studied by MRI" The Journal of Bone & Joint Surgery, vol. 82-B, No. 8 (Nov. 2000), 1196-1198, 3 pages.

Karachalios, et al., "A Mid-Term Clinical Outcome Study of the Advance Medial Pivot Knee Arthroplasty", www.sciencedirect.come, The Knee 16 (2009); 484-488, 5 pages.

Komistek, et al., "In Vivo Flouroscopic Analysis of the Normal Human Knee", Clinical Orthopaedics 410 (2003): 69-81, 13 pages. Komistek, et al., "In Vivo Polyethylene Bearing Mobility Is Maintained in Posterior Stabilized Total Knee Arthroplasty", Clinical Orthopaedics 428 (2004): 207-213, 7 pages.

Koo, et al., "The Knee Joint Center of Rotation Is Predominantly on the Lateral Side During Normal Walking", Journal of Biomechanics, vol. 41 (2008): 1269-1273, 5 pages.

Mannan, et al., "The Medical Rotation Total Knee Replacement: A Clinical and Radiological Review at a Mean Follow-Up of Six Years", The Journal of Bone and Joint Surgery, vol. 91-B, No. 6 (Jun. 2009): 750-756, 7 pages.

Moonot, et al., "Correlation Between the Oxford Knee and American Knee Society Scores at Mid-Term Follow-Up", The Journal of Knee Surgery, vol. 22, No. 3 (Jul. 2009), 226-230, 5 pages.

Murphy, Michael Charles, "Geometry and the Kinematics of the Normal Human Knee", Submitted to Masachusetts Institute of Technology (1990), 379 pages.

Nakagawa, et al., "Tibiofemoral Movement 3: Full Flexion of the Normal Human Knee", J.Bone Joint Surg. Am, vol. 82-B, No. 8 (2000). 1199-1200, 2 pages.

Omori, et al., "The Effect of Geometry of the Tibial Polyethylene Insert on the Tibiofemoral Contact Kinematics in Advance Medical Pivot Total Knee Arthroplasty", The Journal of Orthopaedics Science (2009), 14:754-760, 7 pages.

Shakespeare, et al., "Flexion After Total Knee Replacement. A Comparison Between the Medical Pivot Knee and a Posterior Stabilised Knee", www.sciencedirect.com, The Knee 13 (2006): 371-372, 3 pages.

Walker, et al., "Motion of a Mobile Bearing Knee Allowing Translation of Rotation", Journal of Arthroplasty 17 (2002): 11-19, 9 pages. 2nd Int'l Johnson-Elloy Knee Meeting, Mar. 1987, 9 pages.

Operative Technique, Johnson Elloy Knee System, Chas F. Thackray, Ltd., 1988, 34 pgs.

Operative Technique the Turning Point, Accord, The Johnson/Elloy Concept, Chas FL Thackray Ltd, 32 pages (1990).

Restoration of Soft Tissue Stability, Johnson, et al., Chas. F. Thackray, Ltd., 21 pages (2001).

The Accuracy of Intramedullary Alignment in Total Knee Replacement, Elloy, et al, Chas F. Thackray Ltd, 12 pages (2008).

The Turning Point, Accord, The Johnson Elloy Concept, Chas F. Thackray Ltd, 20 pages (1984).

Prosthesis and Instrumentation the Turning Point, Accord, The Johnson/Elloy Concept, Chas F. Thackray Ltd, 8 pages (1987).

Five to Eight Year Results of the Johnson/Elloy (Accord) Total Knee Arthroplasty, Johnson et al, The Journal of Arthroplasty, vol. 8, No. 1, Feb. 1993, 6 pages.

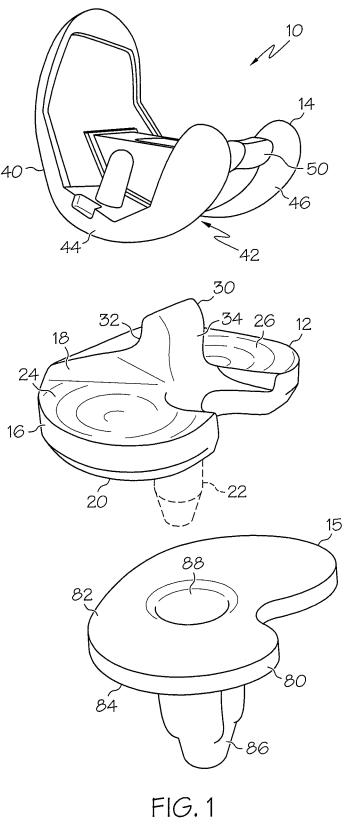
Factors Affecting the Range of Movement of Total Knee Arthroplasty, Harvey et al, The Journal of Bone and Joint Surgery, vol. 75-B, No. 6, Nov. 1993, 6 pages.

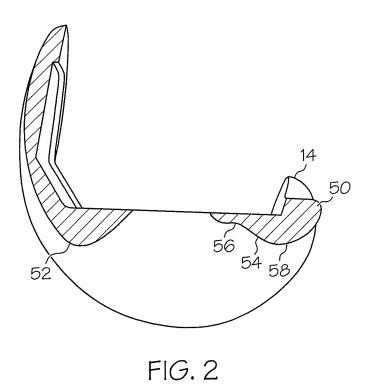
Advice Notice (NI) Mar. 2000, Defect & Investigation Centre, Mar. 13, 2000, 3 pages.

The Johnson Elloy (Accord) Total Knee Replacement, Norton et al, The Journal of Bone and Joint Surgery (BR), vol. 84, No. 6, Aug. 2002, 4 pages.

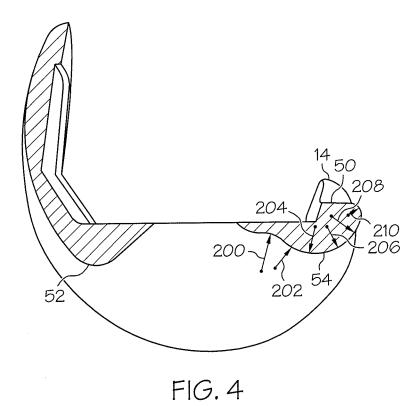
Midvatus Approach in Total Knee Arthroplasty, A Description and a Cadaveric Study Determining The Distance of the Popliteal Artery From the Patellar Margin of the Incision, Cooper et al., The Journal of Arthoplasty, vol. 14 No. 4, 1999, 4 pages.

* cited by examiner





30 62 32-60 34 64 12 FIG. 3



30 224 32 60 222 -220 12

FIG 5

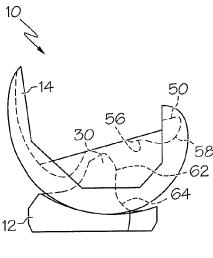


FIG. 6

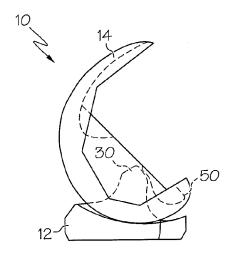


FIG. 7

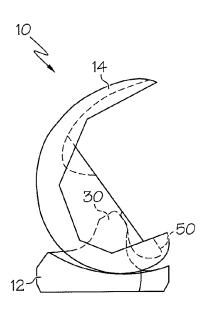


FIG. 8

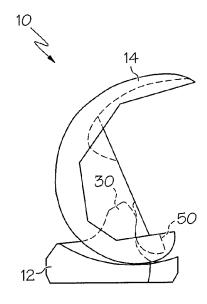
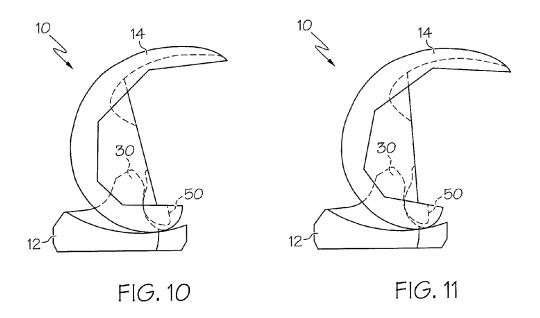
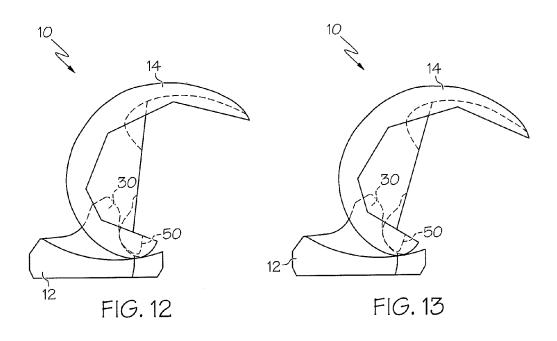


FIG. 9





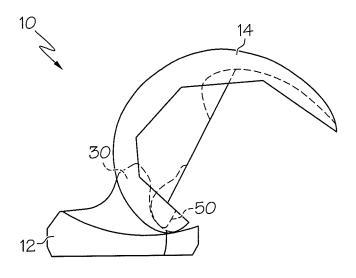


FIG. 14

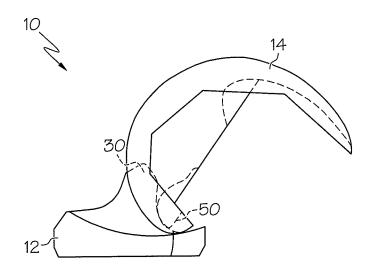
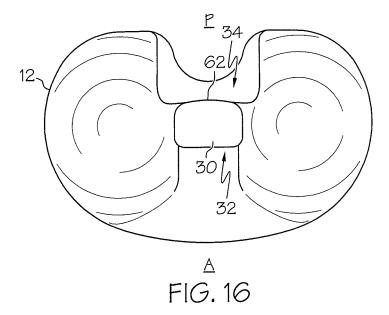
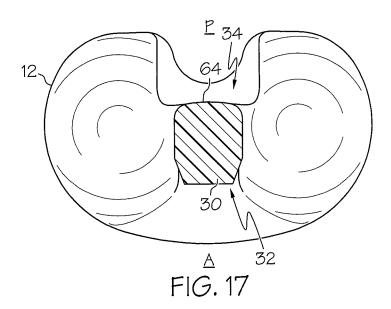
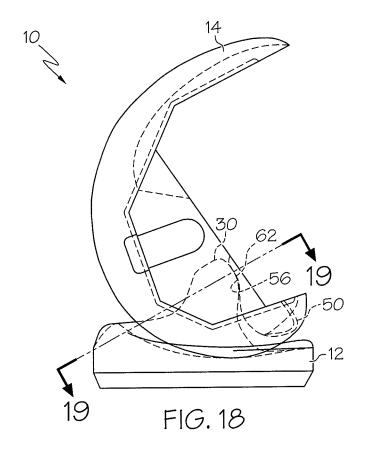
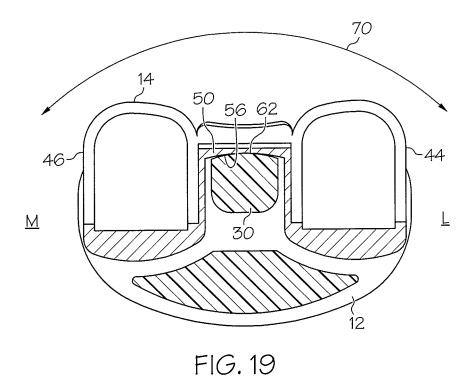


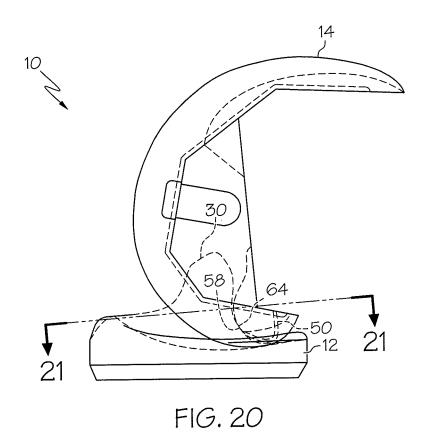
FIG. 15

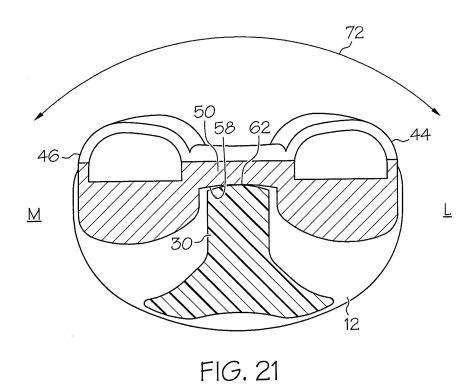


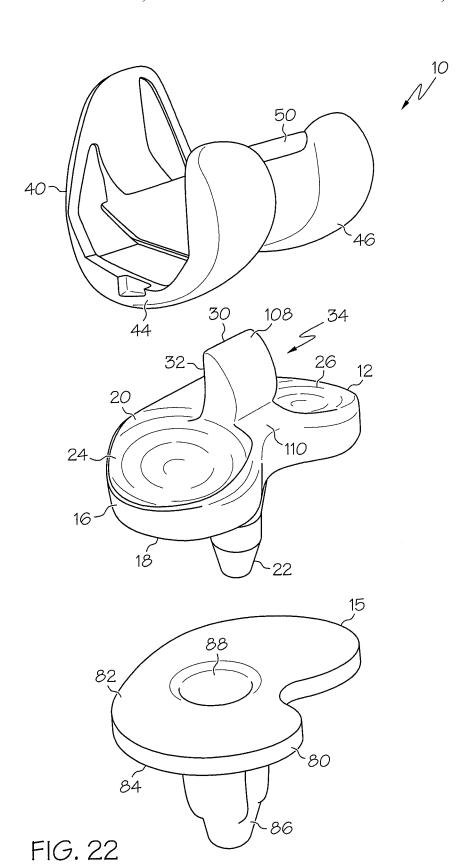












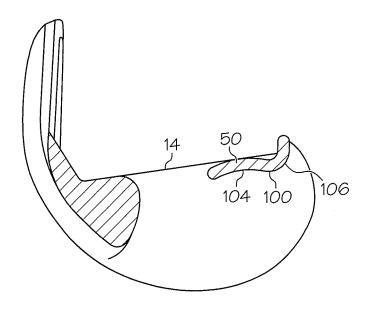


FIG. 23

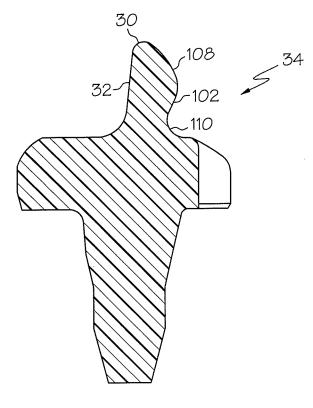
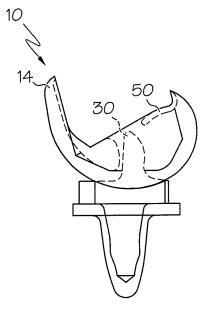


FIG. 24



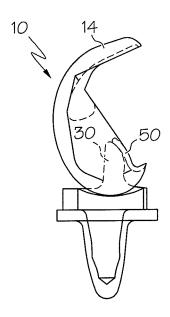


FIG. 25

FIG. 26

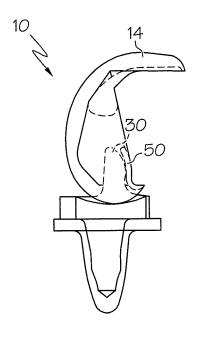


FIG. 27

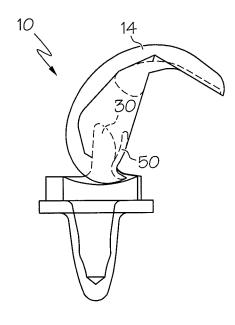


FIG. 28

POSTERIOR STABILIZED ORTHOPAEDIC PROSTHESIS

This application is a continuation of U.S. Utility patent application Ser. No. 13/527,758, which was filed on Jun. 20, 2012 and was a continuation of U.S. Utility patent application Ser. No. 12/165,582 entitled "Posterior Stabilized Orthopaedic Prosthesis," which was filed on Jun. 30, 2008 and issued as U.S. Pat. No. 8,206,451 on Jun. 26, 2012. The entirety of each of those applications is incorporated herein by reference.

CROSS-REFERENCE TO RELATED U.S. PATENT APPLICATION

Cross-reference is made to U.S. Utility patent application Ser. No. 12/165,579 entitled "Orthopaedic Femoral Component Having Controlled Condylar Curvature" by John L. Williams et al., which was filed on Jun. 30, 2008; to U.S. Utility patent application Ser. No. 12/165,574 entitled "Posterior 20 Cruciate-Retaining Orthopaedic Knee Prosthesis Having Controlled Condylar Curvature" by Christel M. Wagner, which was filed on Jun. 30, 2008 and issued as U.S. Pat. No. 8,192,498 on Jun. 5, 2012; and to U.S. Utility patent application Ser. No. 12/165,575 entitled "Posterior Stabilized Ortho-25 paedic Knee Prosthesis Having Controlled Condylar Curvature" by Joseph G. Wyss, which was filed on Jun. 30, 2008 and issued as U.S. Pat. No. 8,187,335 on, May 29, 2012; and to U.S. Utility patent application Ser. No. 12/488,107 entitled "Orthopaedic Knee Prosthesis Having Controlled Condylar 30 Curvature" by Mark A. Heldreth, which was filed on Jun. 19, 2009 and issued as U.S. Pat. No. 8,236,061 on Aug. 7, 2012; the entirety of each of which is incorporated herein by reference.

TECHNICAL FIELD

The present disclosure relates generally to orthopaedic prostheses, and particularly to posterior stabilized orthopaedic prostheses for use in knee replacement surgery.

BACKGROUND

Joint arthroplasty is a well-known surgical procedure by which a diseased and/or damaged natural joint is replaced by 45 a prosthetic joint. A typical knee prosthesis includes a tibial tray, a femoral component, and a polymer insert or bearing positioned between the tibial tray and the femoral component. A knee prosthesis is generally designed to duplicate the natural movement of the patient's joint. However, depending on 50 the severity of the damage to the patient's joint, orthopaedic prostheses of varying mobility may be used. For example, in some patients, the posterior cruciate ligament may be damaged, deficient, or removed during the orthopaedic surgical procedure. In such cases, a posterior stabilized knee orthopaedic prosthesis, which typically restricts or limits the posterior movement of the tibia relative to the femur, may be used.

SUMMARY

According to one aspect, a posterior stabilized knee orthopaedic prosthesis includes a tibial bearing and a femoral component. The tibial bearing may be configured to be coupled to a tibial tray and may include a platform and a spine 65 extending upwardly from the platform. The spine may have a posterior side including a superior and an inferior cam sur-

2

face. The superior cam surface may be embodied as a convex cam surface and the inferior cam surface may be embodied as a concave cam surface. The radius of curvature of the concave cam surface of the spine of the tibial bearing may be substantially equal to or different from the radius of curvature of the convex cam surface of the spine.

In some embodiments, the superior cam surface of the spine of the tibial bearing may be convexly curved in the sagittal plane. Additionally, the inferior cam surface of the spine may be concavely curved in the sagittal plane. Further, in some embodiments, the superior cam surface and the inferior cam surface of the spine may be convexly curved in the transverse plane. In such embodiments, the radius of curvature in the transverse plane of the inferior, concave cam surface of the spine may be substantially equal to or different from the radius of curvature in the transverse plane of the superior, convex cam surface of the spine.

The femoral component of the orthopaedic prosthesis may be configured to articulate with the tibial bearing. The femoral component may include a pair of spaced apart condyles defining an intracondylar notch therebetween and a posterior cam positioned in the intracondylar notch. The posterior cam may include a concave cam surface and a convex cam surface. The tibial bearing and the femoral component are configured such that the concave cam surface of the posterior cam may contact the convex cam surface of the spine during a first range of flexion and the convex cam surface of the posterior cam may contact the concave cam surface of the spine during a second range of flexion. The first range of flexion may be less than the second range of flexion in some embodiments. For example, in one particular embodiment, the first range of flexion is about 50 degrees of flexion to about 80 degrees of flexion and the second range of flexion is about 80 degrees of flexion to about 150 degrees of flexion.

In some embodiments, the spine of the tibial bearing and the posterior cam of the femoral component may each have a substantially "S"-shaped cross-sectional profile. Additionally, in some embodiments, the radius curvature of the convex cam surface of the spine may be greater than the radius of curvature of the concave cam surface of the spine. Further, in such embodiments, the radius of curvature of the concave cam surface of the posterior cam of the femoral component may be substantially greater than the radius of curvature of the convex cam surface of the posterior cam.

According to another aspect, a posterior stabilized knee orthopaedic prosthesis may include a tibial bearing configured to be coupled to a tibial tray and a femoral component configured to be coupled to a surgically-prepared surface of the distal end of a femur. The tibial bearing may include a platform and a spine extending upwardly from the platform. The spine may include a posterior superior cam surface and a posterior inferior cam surface. The posterior superior cam surface may be concave and the posterior inferior cam surface may be convex.

In some embodiments, the radius of curvature of the superior cam surface of the spine of the tibial bearing may be substantially equal to the radius of curvature of the inferior cam surface of the spine. The superior cam surface may be concavely curved in the sagittal plane. Similarly, the inferior cam surface may be convexly curved in the sagittal plane. Additionally, in some embodiments, the superior cam surface of the spine of the tibial bearing may be convexly curved in the sagittal plane and the inferior cam surface of the spine may be concavely curved in the sagittal plane. The posterior inferior cam surface and the posterior superior cam surface of the spine may also be convexly curved in the transverse plane. In such embodiments, the radius of curvature in the transverse

plane of the inferior cam surface of the spine may be substantially equal to or different from the radius of curvature in the transverse plane of the convex cam surface of the spine.

The femoral component may include a posterior cam configured to articulate with the spine of the tibial bearing. The posterior cam may include a concave cam surface and a convex cam surface. In some embodiments, the spine of the tibial bearing and the posterior cam of the femoral component may each have a substantially "S"-shaped cross-sectional profile. Additionally, in some embodiments, the radius curvature of the posterior convex cam surface of the spine may be substantially greater than the radius of curvature of the posterior concave cam surface of the spine and the radius of curvature of the convex cam surface of the posterior cam of 15 tibial bearing of the orthopaedic prosthesis of FIG. 22; and the femoral component is substantially greater than the radius of curvature of the concave cam surface of the posterior cam. The tibial bearing and the femoral component are configured such that the concave cam surface of the posterior cam articulates on the posterior convex cam surface of the spine during 20 a first range of flexion and the convex cam surface of the posterior cam articulates on the posterior concave cam surface of the spine during a second range of flexion greater than the first range of flexion.

According to a further aspect, a posterior stabilized knee 25 orthopaedic prosthesis may include a tibial bearing configured to be coupled to a tibial tray and a femoral component configured to be coupled to a surgically-prepared surface of the distal end of a femur. The tibial bearing may include a platform including a medial bearing surface and a lateral 30 bearing surface. The tibial bearing may also include a spine extending upwardly from the platform between the medial bearing surface and the lateral bearing surface. The spine may include a concave cam surface and a convex cam surface.

The femoral component may include a lateral condyle 35 configured to articulate with the lateral bearing surface of the tibial bearing, a medial condyle configured to articulate with the medial bearing surface, and a posterior cam positioned in an intracondylar notch defined between the lateral condyle and the medial condyle. The posterior cam may include a 40 concave cam surface and a convex cam surface. The concave cam surface of the posterior cam may initially contact the convex cam surface of the spine at a first degree of flexion and the convex cam surface of the posterior cam may initially contact the concave cam surface of the spine at a second 45 degree of flexion greater than the first degree of flexion.

BRIEF DESCRIPTION OF THE DRAWINGS

The detailed description particularly refers to the following 50 figures, in which:

FIG. 1 is an exploded perspective view of one embodiment of an orthopaedic prosthesis;

FIG. 2 is a cross-sectional view of one embodiment of a femoral component of the orthopaedic prosthesis of FIG. 1; 55

FIG. 3 is a cross-sectional view of one embodiment of a tibial bearing of the orthopaedic prosthesis of FIG. 1;

FIG. 4 is another cross-sectional view of the femoral component of FIG. 2;

FIG. 5 is another cross-sectional view of the tibial bearing 60 of FIG. 3;

FIGS. 6-15 are side elevational views of the orthopaedic prosthesis of FIG. 1 at various degrees of flexion;

FIG. 16 is a top plan view of another embodiment of the tibial bearing of the orthopaedic prosthesis of FIG. 1;

FIG. 17 is a cross-sectional plan view of the tibial bearing of FIG. 16 having a portion of the spine removed;

FIG. 18 is a side elevational view of one embodiment of an orthopaedic prosthesis including the tibial bearing of FIG. 16 positioned in an early degree of flexion;

FIG. 19 is a cross-sectional view of the orthopaedic prosthesis of FIG. 18 taken generally along the section line 19-19;

FIG. 20 is a side elevational view of the orthopaedic prosthesis of FIG. 18 positioned in a late degree of flexion;

FIG. 21 is a cross-sectional view of the orthopaedic prosthesis of FIG. 20 taken generally along the section line 21-21;

FIG. 22 is an exploded perspective view of another embodiment of an orthopaedic prosthesis;

FIG. 23 is a cross-sectional view of one embodiment of a femoral component of the orthopaedic prosthesis of FIG. 22;

FIG. 24 is a cross-sectional view of one embodiment of a

FIGS. 25-28 are side elevational views of the orthopaedic prosthesis of FIG. 22 at various degrees of flexion.

DETAILED DESCRIPTION OF THE DRAWINGS

While the concepts of the present disclosure are susceptible to various modifications and alternative forms, specific exemplary embodiments thereof have been shown by way of example in the drawings and will herein be described in detail. It should be understood, however, that there is no intent to limit the concepts of the present disclosure to the particular forms disclosed, but on the contrary, the intention is to cover all modifications, equivalents, and alternatives falling within the spirit and scope of the invention as defined by the appended claims.

Terms representing anatomical references, such as anterior, posterior, medial, lateral, superior, inferior, etcetera, may be used throughout this disclosure in reference to both the orthopaedic implants described herein and a patient's natural anatomy. Such terms have well-understood meanings in both the study of anatomy and the field of orthopaedics. Use of such anatomical reference terms in the specification and claims is intended to be consistent with their well-understood meanings unless noted otherwise.

Referring now to FIG. 1, in one embodiment, a posterior stabilized knee orthopaedic prosthesis 10 includes a tibial insert or bearing 12, a femoral component 14, and a tibial tray 15. The femoral component 14 is configured to articulate with the tibial bearing 12 during use. The tibial bearing 12 is illustratively formed from a polymer material such as a ultrahigh molecular weight polyethylene (UHMWPE), but may be formed from other materials, such as a ceramic material, a metallic material, a bio-engineered material, or the like, in other embodiments. The femoral component 14 and the tibial tray 15 are illustratively formed from a metallic material such as cobalt-chromium or titanium, but may be formed from other materials, such as a ceramic material, a polymer material, a bio-engineered material, or the like, in other embodi-

As discussed in more detail below, the femoral component 14 is configured to articulate with the tibial bearing 12, which is configured to be coupled with the tibial tray 15. The illustrative tibial bearing 12 is embodied as a rotating or mobile tibial bearing and is configured to rotate relative to the tibial tray 15 during use. However, in other embodiments, the tibial bearing 12 may be embodied as a fixed tibial bearing, which may be limited or restricted from rotating relative the tibial tray 15.

The tibial tray 15 is configured to be secured to a surgically-prepared proximal end of a patient's tibia (not shown). The tibial tray 15 may be secured to the patient's tibia via use of bone adhesive or other attachment means. The tibial tray 15

includes a platform 80 having an top surface 82 and a bottom surface 84. Illustratively, the top surface 82 is generally planar and, in some embodiments, may be highly polished. The tibial tray 15 also includes a stem 86 extending downwardly from the bottom surface 84 of the platform 80. A cavity or 5 bore 88 is defined in the top surface 82 of the platform 80 and extends downwardly into the stem 86. The bore 88 is formed to receive a complimentary stem of the tibial bearing 12 as discussed in more detail below.

As discussed above, the tibial bearing 12 is configured to be 10 coupled with the tibial tray 15. The tibial bearing 12 includes a platform 16 having an upper bearing surface 18 and a bottom surface 20. In the illustrative embodiment wherein the tibial bearing 12 is embodied as a rotating or mobile tibial bearing, the bearing 12 includes a stem 22 extending downwardly from the bottom surface 20 of the platform 16. When the tibial bearing 12 is coupled to the tibial tray 15, the stem 22 is received in the bore 88 of the tibial tray 15. In use, the tibial bearing 12 is configured to rotate about an axis defined by the stem 22 relative to the tibial tray 15. In embodiments 20 wherein the tibial bearing 12 is embodied as a fixed tibial bearing, the bearing 12 may or may not include the stem 22 and/or may include other devices or features to secure the tibial bearing 12 to the tibial tray 15 in a non-rotating configuration.

The upper bearing surface 18 of the tibial bearing 12 includes a medial bearing surface 24, a lateral bearing surface 26, and a spine 30 extending upwardly from the platform 16. The medial and lateral bearing surfaces 24, 26 are configured to receive or otherwise contact corresponding medial and lateral condyles 44, 46 of the femoral component 14 as discussed in more detail below. As such, the bearing surfaces 24, 26 may have concave contours in some embodiments. The spine 30 is positioned between the bearing surfaces 24, 26 and includes an anterior side 32 and a posterior side 34.

The femoral component 14 is configured to be coupled to a surgically-prepared surface of the distal end of a patient's femur (not shown). The femoral component 14 may be secured to the patient's femur via use of bone adhesive or other attachment means. The femoral component 14 includes 40 an articulating surface 40 having a pair of spaced apart medial and lateral condyles 44, 46. In use, the condyles 44, 46 replace the natural condyles of the patient's femur and are configured to articulate on the corresponding bearing surfaces 24, 26 of the platform 16 of the tibial bearing 12.

The condyles 44, 46 are spaced apart to define an intracondyle notch or recess 42 therebetween. A posterior cam 50 and an anterior cam 52 (see FIG. 2) are positioned in the intracondyle notch 42. The posterior cam 50 is located toward the posterior side of the femoral component 14 and is configured to engage or otherwise contact the spine 30 of the tibial bearing 12 during flexion as illustrated in and described in more detail below in regard to FIGS. 4-13.

Referring now to FIGS. 2-5, each of the posterior cam 50 of the femoral component 14 and the spine 30 of the tibial 55 bearing 12 have a substantially "S"-shaped cross-sectional profile in the sagittal plane. In particular, as shown in FIG. 2, the posterior cam 50 of the femoral component 14 includes a cam surface 54 configured to contact a cam surface 60 of the spine 30 during use. To do so, the cam surface 54 of the 60 posterior cam 50 includes a concave cam surface 56 and a convex cam surface 58. In the illustrative embodiment, the convex cam surface 56. The cam surfaces 56, 58 may have similar or different radius of curvatures. For example, in some 65 embodiments, the convex cam surface 58 may have a radius of curvature substantially larger than the radius of curvature

6

of the concave cam surface **56**. However, in other embodiments, the convex cam surface **58** may have a radius of curvature that is substantially equal to or less than the radius of curvature of the concave cam surface **56**.

In some embodiments, the curvature of the cam surfaces 56, 58 may be defined by a single radius of curvature. The particular radius of curvature of the cam surfaces 56, 58 (i.e., the "size" of the cam surfaces) may be dependent upon a number of criteria such as the size of the implant, the shape or geometry of the articulating surface of the spine 30 of the tibial implant 12, and/or the like. In other embodiments, however, the concave cam surface 56 and the convex cam surface 58 of the femoral component 14 may be formed from multiple radii of curvature. For example, in the embodiment illustrated in FIG. 4, the concave cam surface 56 is defined by a radius of curvature 200 and a radius of curvature 202, each of which is tangent to the other. In one particular embodiment, the radius of curvature 200 is about 10.42 millimeters and the radius of curvature 202 is about 8.13 millimeters. Additionally, the convex cam surface 58 is defined by a plurality of radii of curvature 204, 206, 208, and 210. Each of the radii of curvature 204, 206, 208, 210 is tangent with the each adjacent radius of curvature. In one particular embodiment, the radius of curvature 204 is about 7.14 millimeters, the radius of curvature 206 is about 7.01 millimeters, the radius of curvature 208 is about 7.30 millimeters, and the radius of curvature 210 is about 2.30 millimeters. In other embodiments, a larger or lesser number of radii of curvature may be used define the cam surfaces 56, 58. Additionally, the radii of curvature 200, 202, 204, 206, 208, 210 may have other values in other embodiments.

Referring now to FIG. 3, the cam surface 60 of the tibial bearing 12 is defined on the posterior side 34 of the spine 30. Similar to the cam surface 54 of the posterior cam 50 of the femoral component 14, the cam surface 60 of the spine 30 includes a convex cam surface 62 and a concave cam surface 64. In the illustrative embodiment, the convex cam surface 62 is positioned superiorly relative to the concave cam surface 64. Similar to the cam surfaces 56, 58 of the posterior cam 50, the cam surfaces 62, 64 of the spine 30 may have similar or different radius of curvatures. For example, in some embodiments, the concave cam surface 64 has a radius of curvature substantially larger than the radius of curvature of the convex cam surface 62. However, in other embodiments, the concave cam surface 64 may have a radius of curvature that is substantially equal to or less than the radius of curvature of the convex cam surface 62.

In some embodiments, the curvature of the cam surfaces 62, 64 may be defined by a single radius of curvature. The particular radius of curvature of the cam surfaces 62, 64 (i.e., the "size" of the cam surfaces) may be dependent upon a number of criteria such as the size of the implant, the shape or geometry of the articulating surface of the posterior cam 50 of the femoral component 14, and/or the like. In other embodiments, however, the convex cam surface 62 and the concave cam surface 64 of the tibial bearing 12 may be formed from multiple radii of curvature. For example, in the embodiment illustrated in FIG. 5, the concave cam surface 64 is defined by a radius of curvature 220 and a radius of curvature 222, each of which is tangent to the other. In one particular embodiment, the radius of curvature 220 is about 9.00 millimeters and the radius of curvature 222 is about 13.00 millimeters. The convex cam surface 62 is defined by a radius of curvature 224. In one particular embodiment, the radius of curvature 224 is about 8.00 millimeters. Of course, in other embodiments, a larger or lesser number of radii of curvature may be used

define the cam surfaces **62,64**. Additionally, the radii of curvature **220**, **222**, **224** may have other values in other embodiments

Referring now to FIGS. 6-15, the femoral component 14 and the tibial bearing 12 are configured such that the posterior 5 cam 50 of the femoral component 14 contacts the spine 30 of the tibial bearing 12 during flexion. In particular, during early flexion, the concave cam surface 56 of the posterior cam 50 contacts the convex cam surface 62 of the spine 30. As flexion of the orthopaedic prosthesis 10 is increased, the contact 10 between the posterior cam 50 and the spine 30 transitions from contact between the concave cam surface 56 of the posterior cam 50 and the convex cam surface 62 of the spine 30 to contact between the convex cam surface 64 of the spine 30 to contact between the concave surface 64 of the spine 30 during late flexion.

As shown in FIG. 6, when the orthopaedic prosthesis 10 is in extension or is otherwise not in flexion (e.g., a flexion of about 0 degrees), the posterior cam 50 is not in contact with the spine 30. However, during early flexion as illustrated in 20 FIGS. 7 and 8, the posterior cam 50 of the femoral component 14 contacts the spine 30 of the tibial bearing 12. For example, in one embodiment as illustrated in FIG. 7, as the orthopaedic prosthesis 10 is moved in flexion, the concave cam surface 56 of the posterior cam 50 initially contacts the convex cam 25 surface 62 of the spine at a predetermined degree of flexion. In the illustrative embodiment, the femoral component 14 and the tibial bearing 12 are configured such that the cam surfaces 56, 62 initially contact each other at about 60 degrees of flexion. However, in other embodiments, the degree of flexion 30 at which initial contact between the posterior cam 50 and the spine 30 is established may be determined based on particular criteria such as the size of the orthopaedic prosthesis 10, the shape or geometry of the articulating surface of the femoral component 14 and/or the tibial bearing 12, and/or the like.

During early flexion of the orthopaedic prosthesis 10, contact between the concave cam surface 56 and the convex cam surface 62 is maintained. For example, in one embodiment as shown in FIG. 8, the convex cam surface 62 of the spine 30 may be fully "seeded" in the concave cam surface 56 of the 40 posterior cam 50 at about 60 degrees of flexion. After early flexion, the contact between the posterior cam 50 and the spine 30 transitions from the cam surfaces 56, 62 to the cam surfaces 58, 64. For example, in one embodiment as illustrated in FIG. 9, the contact between the posterior cam 50 and 45 the spine 30 begins transitioning to the cam surfaces 58, 64 at about 80 degrees. At this degree of flexion, initial contact between the convex cam surface 58 of the posterior cam 50 and the concave cam surface 64 of the spine 30 may be established.

During late flexion of the orthopaedic prosthesis 10, the convex cam surface 58 maintains contact with the concave cam surface 64. For example, FIGS. 10-15 illustrate one embodiment at various degrees of late flexion. In particular, the orthopaedic prosthesis 10 is illustrated at about 100 55 degrees of flexion in FIG. 10, at about 110 degrees of flexion in FIG. 11, at about 120 degrees of flexion in FIG. 12, at about 130 degrees of flexion in FIG. 13, at about 140 degrees of flexion in FIG. 14, and at about 150 degrees of flexion in FIG. 15.

It should be appreciated that contact between the posterior cam 50 and the spine 30 is maintained throughout the range of early and late flexion. The particular range of early flexion (i.e., the range at which the concave cam surface 56 of the posterior cam 50 contacts the convex cam surface 62 of the 65 spine 30) and late flexion (i.e., the range at which the convex cam surface 58 of the posterior cam 50 contacts the concave

8

cam surface 64 of the spine 30) of the orthopaedic prosthesis 10 may be dependent upon one or more criteria such as the size of the orthopaedic prosthesis 10, the shape or geometry of the articulating cam surfaces of the tibial bearing 12 and the femoral component 14, or the like. In the illustrative embodiment, the orthopaedic prosthesis 10 is configured to have an early flexion range of about 50 degrees to about 80 degrees and a late flexion range of about 80 degrees to about 150 degrees, but other ranges of flexion may be used in other embodiments. The range of early and late flexion of the orthopaedic prosthesis 10 is determined, in part, based on the radius of curvature of the cam surface 56, 58, 62, 64. As such, the range of early and late flexion of the orthopaedic prostheses 10 may be configured by adjusting the radius of curvature of the cam surfaces 56, 58, 62, 64.

It should also be appreciated that because the cam surface 54 of the posterior cam 50 includes the concave cam surface 56 and the convex cam surface 58 and the cam surface 34 of the spine 30 includes the convex cam surface 62 and the concave cam surface 64, the contact surface area between the posterior cam 50 and the spine 30 is increased through the flexion range relative to orthopaedic prostheses wherein the posterior cam and/or the spine include planar cam surfaces or cam surfaces having only a concave or convex surface. For example, the contact area between the posterior cam 50 and the spine 30 is increased in early flexion due to the interface between the concave cam surface 56 of the posterior cam 50 and the convex cam surface 62 of the spine 30. Additionally, in late flexion, the contact area between the posterior cam 50 and the spine 30 is increased in later degrees of flexion due to the interface between the convex cam surface 58 of the posterior cam 50 and the concave cam surface 64 of the spine 30. Because the contact between the posterior cam 50 and the spine 30 is spread across a greater contact area, the anterior wear of the spine 30 may also be decreased.

Referring now to FIGS. 16 and 17, in some embodiments, the posterior side 34 of the spine 30 may also be curved in the transverse plane. That is, each of the superior, convex cam surface 62 and the inferior, concave cam surface 64 may be convex in the transverse plane direction. For example, as illustrated in FIG. 16, the convex cam surface 62 of the spine 30 may be convexly curved in the transverse plane. Additionally, as illustrated in FIG. 17, the concave cam surface 64 of the spine 30 may be convexly curved in the transverse plane. The radius of curvature in the transverse plane of the convex cam surface 62 and the concave cam surface 64 may be substantially equal or different. For example, in some embodiments, the radius of curvature in the transverse plane of the concave cam surface 64 may be greater than the radius of curvature in the transverse plane of the convex cam surface 62. Alternatively, in other embodiments, the radius of curvature in the transverse plane of the convex cam surface 62 may be greater than the radius of curvature in the transverse plane of the concave cam surface **64**.

In embodiments wherein the cam surfaces 62, 64 of the spine 30 are curved in the transverse plane, the posterior cam 50 of the femoral component 14 articulates on the cam surfaces 62, 64 in the transverse plane such that the femoral component 14 rotates an amount about the spine 30. For example, as illustrated in FIGS. 18 and 19, when the concave cam surface 56 of the posterior cam 50 is in contact with the convex cam surface 62 of the spine 30 during early flexion, the femoral component 14 may rotate about the spine 30 in a generally medial-lateral direction in the transverse plane as indicated by arrow 70. In such embodiments, the concave cam surface 56 of the posterior cam 50 may be substantially planar in the medial-lateral direction in some embodiments.

Alternatively, similar to the convex cam surface 62 of the spine 30, the concave cam surface 56 of the posterior cam 50 of the femoral component 14 may also be curved in the medial-lateral direction. For example, as illustrated in FIG. 19, the concave cam surface 56 may be concavely curved in 5 the medial-lateral direction. In some embodiments, the radius of curvature in the medial-lateral direction of the concave cam surface 56 may be substantially equal to the radius of curvature in the transverse plane of the convex cam surface 62 of the spine 30. Alternatively, the radius of curvature in the medial-lateral direction of the concave cam surface 56 may be greater or less than the radius of curvature in the transverse plane of the convex cam surface 62. The amount of rotation between the femoral component 14 and the tibial bearing 12 during early flexion may be adjusted based on the radius of curvatures in the transverse plane of the cam surfaces 56, 62. For example, an increased amount of rotation during early flexion of the orthopaedic prosthesis may be obtained by decreasing the radius of curvature in the transverse plane of the convex cam surface 62.

Referring now to FIGS. 20 an 21, when the convex cam surface 58 of the posterior cam 50 is in contact with the concave cam surface 64 of the spine 30 during late flexion, the femoral component 14 may rotate about the spine 30 in a generally medially-laterally direction in the transverse plane 25 as indicated by arrow 72 in some embodiments. In such embodiments, the convex cam surface 58 of the posterior cam 50 may be substantially planar in the medial-lateral direction. Alternatively, similar to the concave cam surface 64 of the spine 30, the convex cam surface 58 of the posterior cam 50 of 30 the femoral component 14 may be curved in the mediallateral direction. For example, as illustrated in FIG. 21, the convex cam surface 58 may be concavely curved in the medial-lateral direction. In some embodiments, the radius of curvature in the medial-lateral direction of the convex cam 35 surface 58 may be substantially equal to the radius of curvature in the medial-lateral direction of the concave cam surface 64 of the spine 30. Alternatively, the radius of curvature in the medial-lateral direction of the convex cam surface 58 may be greater or slightly less than the radius of curvature in the 40 medial-lateral direction of the concave cam surface 64. As discussed above in regard to early flexion, the amount of rotation between the femoral component 14 and the tibial bearing 12 during late flexion may be adjusted based on the radius of curvatures in the medial-lateral direction of the cam 45 surfaces 58, 64

As discussed above, the range of late flexion of the illustrative orthopaedic prosthesis 10 is greater than the range of early flexion. However, in other embodiments, the orthopaedic prosthesis 10 may have a range of early flexion that is 50 greater than the range of late flexion. That is, because the range of early and late flexion of the orthopaedic prosthesis is determined, in part, based on the radius of curvature of the cam surface 56, 58, 62, 64, the range of early and late flexion may be adjusted by changing the radius of curvature of the 55 cam surfaces 56, 58, 62, 64 (i.e., the "size" of the cam surfaces). For example, as illustrated in FIGS. 22-28, in another embodiment, the orthopaedic prosthesis 10 may include an early flexion range (i.e., the range at which the concave cam surface of the posterior cam 50 contacts the convex cam 60 surface of the spine 30) that is greater than the late flexion (i.e., the range at which the convex cam surface of the posterior cam 50 contacts the concave cam surface of the spine 30).

In such embodiments, as illustrated in FIGS. 22-24, the posterior cam 50 of the femoral component 14 includes a cam 65 surface 100 configured to contact a cam surface 102 of the spine 30 during use. To do so, the cam surface 100 of the

10

posterior cam 50 includes a concave cam surface 104 and a convex cam surface 106. In the illustrative embodiment, the convex cam surface 106 is positioned posteriorly to the concave cam surface 104. The concave cam surface 104 has a radius of curvature substantially larger than the radius of curvature of the convex cam surface 106. As discussed above in regard to the cam surfaces 56, 58, the particular radius of curvature of the cam surfaces 104, 106 (i.e., the "size" of the cam surfaces) may be dependent upon a number of criteria such as the size of the implant, the shape or geometry of the articulating surface of the femoral component 14 and/or the tibial bearing 12, and/or the like. In one particular embodiment, the concave cam surface 104 has a radius of curvature of about 12.7 millimeters and the convex cam surface 106 has a radius curvature of about 6.4 millimeters

Similar to the cam surface 100 of the posterior cam 50 of the femoral component 14, the cam surface 102 of the spine 30 includes a convex cam surface 108 and a concave cam surface 110. In the illustrative embodiment, the convex cam surface 108 is positioned superiorly relative to the concave cam surface 110. The convex cam surface 108 has a radius of curvature substantially larger than the radius of curvature of the concave cam surface 110. Again, the particular radius of curvature of the cam surfaces 108, 110 (i.e., the "size" of the cam surfaces) may be dependent upon a number of criteria such as the size of the implant, the patient's anatomy, and/or the like. In one particular embodiment, the convex cam surface 108 has a radius of curvature of about 10.3 millimeters and the concave cam surface 110 has a radius curvature of about 1.00 millimeters.

Because radius of curvature of the cam surfaces 104, 108 are greater than the radius of curvature of the cam surfaces 106, 110, the range of early flexion of the embodiment of the orthopaedic prosthesis 10 illustrated in FIGS. 22-28 is greater than the range of late flexion. For example, as shown in FIG. 25, when the orthopaedic prosthesis 10 is in extension or is otherwise not in flexion (e.g., a flexion of about 0 degrees), the posterior cam 50 is not in contact with the spine 30. However, during early flexion as illustrated in FIG. 26, the posterior cam 50 of the femoral component 14 contacts the spine 30 of the tibial bearing 12. That is, during early flexion, the concave cam surface 104 of the posterior cam 50 contacts the convex cam surface 108 of the spine 30. Because the radius of curvature of the cam surfaces 104, 108 are increased, the cams surfaces 104, 108 maintain contact with each other through a larger range of flexion. As such, the range of early flexion of the orthopaedic prosthesis is increased relative to embodiments wherein the radius of curvature of the cam surfaces 104, 108 is decreased. After early flexion, the contact between the posterior cam 50 and the spine 30 transitions from the cam surfaces 104, 108 to the cam surfaces 106, 110. For example, in one embodiment as illustrated in FIG. 27, the contact between the posterior cam 50 and the spine 30 beings transitioning to the cam surfaces 106, 110. At this degree of flexion, initial contact between the convex cam surface 106 of the posterior cam 50 and the concave cam surface 110 of the spine 30 may be established. Subsequently, during late flexion of the orthopaedic prosthesis 10, the convex cam surface 106 maintains contact with the concave cam surface 110 as illustrated in FIG. 28.

Again, it should be appreciated that contact between posterior cam 50 and the spine 30 is maintained throughout the range of early and late flexion. The particular range of early flexion (i.e., the range at which the concave cam surface 104 of the posterior cam 50 contacts the convex cam surface 108 of the spine 30) and late flexion (i.e., the range at which the convex cam surface 106 of the posterior cam 50 contacts the

concave cam surface 110 of the spine 30) of the orthopaedic prosthesis 10 may be dependent upon one or more criteria such as the size of the orthopaedic prosthesis 10, the patient's anatomy, or the like. In the illustrative embodiment of FIGS. 22-28, the orthopaedic prosthesis is configured to have an 5 early flexion range of about 50 degrees to about 100 degrees and a late flexion range of about 100 degrees to about 150 degrees, but other ranges of flexion may be used in other embodiments.

It should also be appreciated that because the cam surface 10 100 of the posterior cam 50 includes the concave cam surface 104 and the convex cam surface 106 and the cam surface 102 of the spine 30 includes the convex cam surface 108 and the concave cam surface 110, the contact surface area between the posterior cam 50 and the spine 30 is increased relative to 15 orthopaedic prostheses wherein the posterior cam and/or the spine include planar cam surfaces or cam surfaces having only a concave or convex surface. In particular, because the concave cam surface 104 of the posterior cam 50 and the convex cam surface 108 of the spine 30 each have large radius 20 of curvatures, the contact area between the posterior cam 50 an the spine 30 is increased during early flexion. Additionally, as discussed above, because the contact between the posterior cam 50 and the spine 30 is spread across a greater contact area, the anterior wear of the spine 30 may also be decreased. 25

While the disclosure has been illustrated and described in detail in the drawings and foregoing description, such an illustration and description is to be considered as exemplary and not restrictive in character, it being understood that only illustrative embodiments have been shown and described and 30 that all changes and modifications that come within the spirit of the disclosure are desired to be protected.

There are a plurality of advantages of the present disclosure arising from the various features of the devices and assemblies described herein. It will be noted that alternative 35 embodiments of the devices and assemblies of the present disclosure may not include all of the features described yet still benefit from at least some of the advantages of such features. Those of ordinary skill in the art may readily devise incorporate one or more of the features of the present invention and fall within the spirit and scope of the present disclosure as defined by the appended claims.

The invention claimed is:

- 1. An orthopaedic prosthesis comprising:
- a tibial bearing configured to be coupled to a tibial tray, the tibial bearing having a platform and a spine extending upwardly from the platform, the spine having a posterior side including a cam surface having a first section that is convexly curved in the sagittal plane and a second sec- 50 tion that is concavely curved in the sagittal plane, and
- a femoral component configured to articulate with the tibial bearing, the femoral component including (i) a pair of spaced apart condyles defining an intracondylar notch therebetween, (ii) a posterior cam positioned at a poste- 55 rior end of the intracondylar notch, the posterior cam including a cam surface having an anterior section that is concavely curved in the sagittal plane and a posterior section that is convexly curved in the sagittal plane, and (iii) an anterior surface positioned at an anterior end of 60 the intracondylar notch such that the intracondylar notch includes an opening defined between the posterior cam and the anterior surface,

wherein (i) during a first range of flexion starting at greater than or equal to 0 degrees of flexion, the posterior cam is 65 spaced apart from the spine, (ii) during a second range of flexion starting at greater than or equal to 50 degrees of

12

flexion, the anterior section of the cam surface of the posterior cam contacts only the first section of the cam surface of the spine and posterior section of the cam surface of the posterior cam is spaced apart from the spine, (iii) during a third range of flexion starting at greater than or equal to 80 degrees of flexion, the anterior section of the cam surface of the posterior cam contacts the first section of the cam surface of the spine and posterior section of the cam surface of the posterior cam contacts the second section of the cam surface of the spine, and (iv) during a fourth range of flexion starting at greater than or equal to 100 degrees of flexion, the anterior section of the cam surface of the posterior cam is spaced apart from the spine and the posterior section of the cam surface of the posterior cam contacts only the second section of the cam surface of the spine.

- 2. The orthopaedic prosthesis of claim 1, wherein the spine of the tibial bearing and the posterior cam of the femoral component each have a substantially "S"-shaped cross-sectional profile.
- 3. The orthopaedic prosthesis of claim 1, wherein the first section of the cam surface of the spine of the tibial bearing is located superiorly relative to the second section of the cam surface of the spine.
- 4. The orthopaedic prosthesis of claim 1, wherein the first range of flexion is about 0 degrees of flexion to about 50 degrees of flexion.
- 5. The orthopaedic prosthesis of claim 1, wherein the second range of flexion is about 50 degrees of flexion to about 80 degrees of flexion.
- **6**. The orthopaedic prosthesis of claim **1**, wherein the third range of flexion is about 80 degrees of flexion to about 100 degrees of flexion.
- 7. The orthopaedic prosthesis of claim 1, wherein the first section of the spine of the tibial bearing is defined by a first radius of curvature and the second section of the spine is defined by a second radius of curvature different from the first radius of curvature.
- 8. The orthopaedic prosthesis of claim 1, wherein the antetheir own implementations of the devices and assemblies that 40 rior section the posterior cam of the femoral component is defined by a first radius of curvature and the posterior section of the posterior cam is defined by a second radius of curvature different from the first radius of curvature.
 - 9. The orthopaedic prosthesis of claim 1, wherein:
 - the anterior section of the cam surface of the posterior cam is a first anterior section, and
 - the cam surface of the posterior cam includes a second anterior section positioned anterior of the first anterior section, the second anterior section being convexly curved in the sagittal plane.
 - 10. An orthopaedic prosthesis comprising:
 - a tibial bearing configured to be coupled to a tibial tray, the tibial bearing having a platform including a medial bearing surface and a lateral bearing surface and a spine extending upwardly from the platform between the medial bearing surface and the lateral bearing surface, the spine having a posterior side including a cam surface having a first section that is convexly curved in the sagittal plane and convexly curved in the transverse plane, and a second section that is concavely curved in the sagittal plane and convexly curved in the transverse plane, and
 - a femoral component configured to articulate with the tibial bearing, the femoral component including (i) a pair of spaced apart condyles defining an intracondylar notch therebetween, (ii) a posterior cam positioned at a posterior end of the intracondylar notch, the posterior cam

including a cam surface having an anterior section that is concavely curved in the sagittal plane and a posterior section that is convexly curved in the sagittal plane, and (iii) an anterior surface positioned at an anterior end of the intracondylar notch such that the intracondylar notch includes an opening defined between the posterior cam and the anterior surface,

wherein (i) at a flexion angle of about 0 degrees of flexion, the posterior cam is disengaged from the spine, (ii) only the anterior section of the cam surface of the posterior cam contacts the first section of the cam surface of the spine during a first range of flexion starting at a flexion angle of at least about 50 degrees, and (iii) contact between the posterior cam and the spine transitions to contact between the posterior section of the cam surface of the posterior cam and the second section of the cam surface of the spine in a second range of flexion starting at a flexion angle of at least 80 degrees,

14

wherein the first section of the cam surface of the spine of the tibial bearing is located superiorly relative to the second section of the cam surface of the spine,

wherein the spine of the tibial bearing and the posterior cam of the femoral component each have a substantially "S"-shaped cross-sectional profile in the sagittal plane.

11. The orthopaedic knee joint prosthesis of claim 10, wherein the first range of flexion is about 50 degrees of flexion to about 80 degrees of flexion and the second range of flexion is about 80 degrees of flexion to about 150 degrees of flexion.

12. The orthopaedic prosthesis of claim 10, wherein the anterior section of the cam surface of the posterior cam is a first anterior section, and the cam surface of the posterior cam includes a second anterior section positioned anterior of the first anterior section, the second anterior section being convexly curved in the sagittal plane.

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